WIND TURBINES and EARTHQUAKES



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WIND TURBINES and EARTHQUAKES

- Introduction
- Modal Approach
- Time-Domain Simulation of Earthquakes
- Results for Nordex N80 in Ryuyo-Cho (Japan)
- Conclusions





- Wind loads : Wind turbines designed to withstand aerodynamic forces on rotor
- Wind farms in areas with strong earthquakes
- Earthquake: ground motion leads to structural vibrations and loads, earthquake loads should not exceed design loads
- Consequence: earthquake loads have to be calculated in order to assess whether a given wind turbine is suitable for a site or whether design modifications are necessary













- Wind turbines made from elastic materials like steel and fibre reenforced plastic
- Low structural damping











Theoretical concept to describe effects on structures:

Single degree of freedom (SDOF) oscillator

- characterized by
- mass M
- stiffness K
- and resulting frequency Ω or period T





• Standards (Eurocode 8): SDOF Oscillator response spectrum





Modal Approach

- Tower approximated as system of lumped masses
- Nacelle and rotor as point mass at tower top
- Vibration modes can be calculated
- Tower modes can be regarded as SDOF oscillators



Modal Approach



- With modes and SDOF oscillator spectrum forces and moments in the tower are obtained
- Additional wind loads on turbine taken into account





Time Domain Simulation





Time Domain Simulation





Flex5 - multi body and modal dynamics (S. Øye, DTU)

- 2 modes flapwise and 2 edgewise for blades
- drive train rotation and torsion ...
- more than 20 degrees of freedom
- time-domain dynamic equation integrated
- sectional loads are obtained
- takes into account wind and functional loads in realistic fashion



Time Domain Simulation



- Generate 3-D synthetic accelerograms that are consistent with SDOF oscillator response spectrum
- Specified in Standards e.g. Eurocode 8
- Include accelerograms in simulation program





Results for Nordex N80





- Rotor diameter 80 m
- Rated power 2500 kW, variable speed, pitch-regulated
- Hub height Ryuyo Cho 60 m
- Certified for IEC1A site





Results for Nordex N80

11 NGen generator speed 321.98/ 491.22/ -8.42/1242.34 rpm 1,000 500 k₩ electrical power 378.16/ 757.35/ 0.00/2102.13 12 P 2,000 1,500 1,000 500 L.C 23 MBB1 kNm bending moment YZ B1 R=1765.36/344.01/ 61.26/2269.03 2,000 -1,500 1,000 Marahanninn 500 43 FSN kΝ 450.69/106.90/70.09/830.11 main bearing XY shear 800 600 400 200 67 FSK2 kΝ yaw bearing YZ shear 200.99/106.12/ 0.94/590.08 400 200 yaw bearing YZ bending 1704.98/ 886.69/ 148.64/5723.7 71 MBK2 kNm 4,000 2,000 Ŵ 14/: 45 50 -5 10 15 20 25 30 35 40

DLC 5.1b_q000 emergency shut down at v=25 m/s

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Engineering GmbH

Results for Nordex N80

- Example: bending moments in the tower
- Detailed picture of blade and machine loads
- Earthquake loads are covered by design loads
- Vertical component taken into account, leads to extreme values
- 0.3 g is upper limit for peak ground acceleration





Conclusions



- Modal approach and time-domain simulation (Flex5) compared
- Simulation leads to much more detailed information on loads on the structure near and above tower top
- Realistic combination of ground acceleration, wind forces and functional loads (shut down)
- Results show that especially loads near tower top are underestimated by modal analysis
- Time-domain simulation recommended for sites with earthquakes of magnitude VII or more on the modified Mercalli scale

